

# Beam Loading Studies in BEPC2

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Teytelman<sup>3</sup>

<sup>1</sup>IHEP, Beijing, China

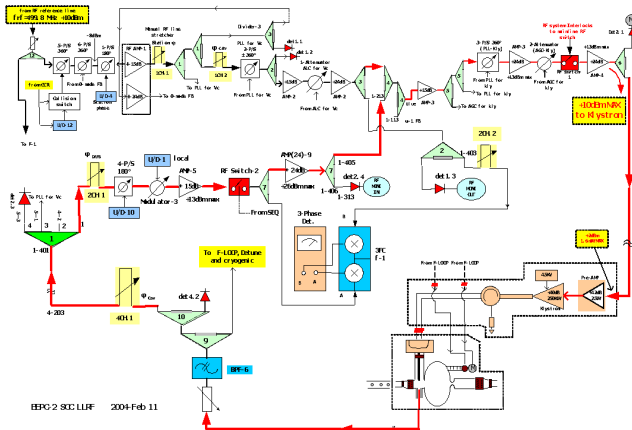
<sup>2</sup>JLAB, Newport News, VA, USA

<sup>3</sup>Dimtel, Inc., San Jose, CA, USA

December 18, 2016

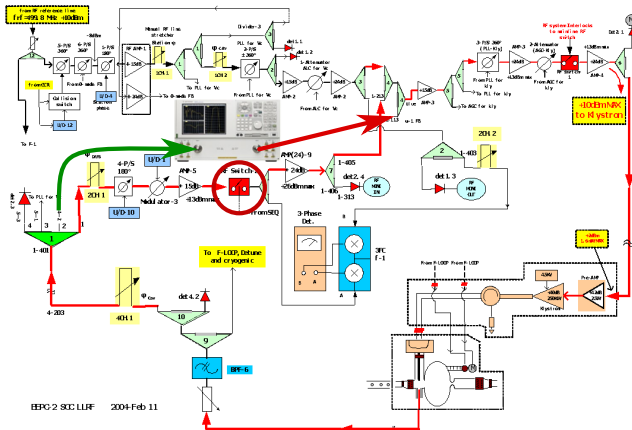


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- The goal is to estimate direct loop gain at the nominal operating point;
- A difficult measurement — need to detect small NWA excitation in presence of large RF fundamental signal;
  - Field setpoint 222 kV — as low as possible to reduce fundamental signal;
  - Cavity detuned by setting load angle offset to  $-40^\circ$ ;
  - Amplitude and phase loops turned off;
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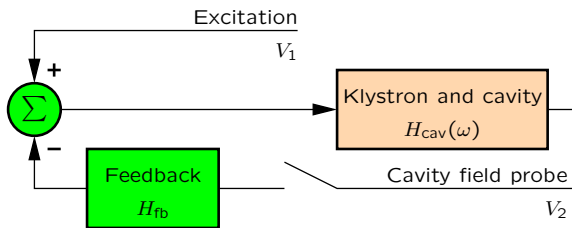


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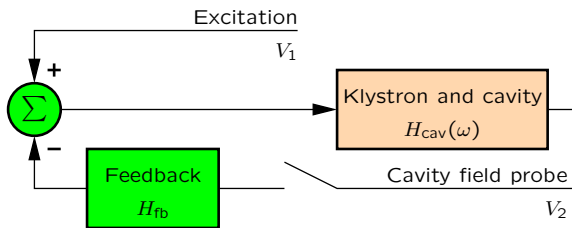


# System Model



- Cavity response:  $H_{\text{cav}}(\omega) = \frac{2i\sigma\omega}{\omega^2 - 2i\sigma\omega - \omega_r^2} G e^{-i(\omega - \omega_r)\tau} e^{i\phi_0}$
- Five parameters: gain  $G$ , damping rate  $\sigma$ , center frequency  $\omega_r$ , delay  $\tau$ , and phase shift  $\phi_0$ ;
- Feedback response is just gain and phase shift:  $H_{\text{fb}}(\omega) = G_{\text{fb}} e^{i\phi_{\text{fb}}}$ ;
- In open loop estimate the parameters of  $H_{\text{cav}}(\omega)$ ;
- Two parameter fit ( $G_{\text{fb}}, \phi_{\text{fb}}$ ) to the closed-loop  $S_{21}(\omega)$ .

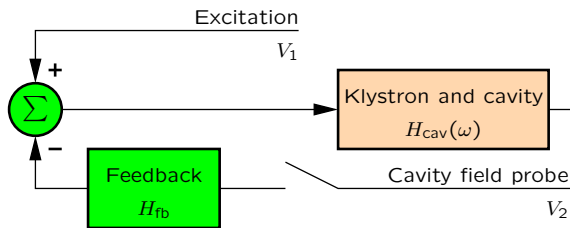
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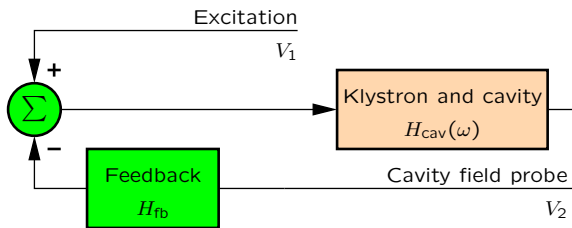


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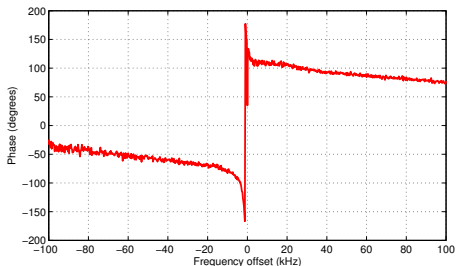
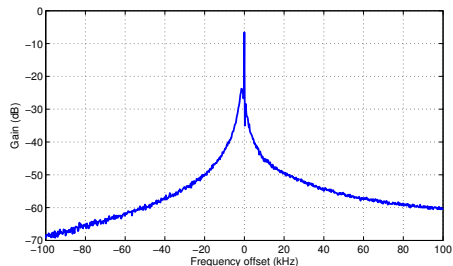
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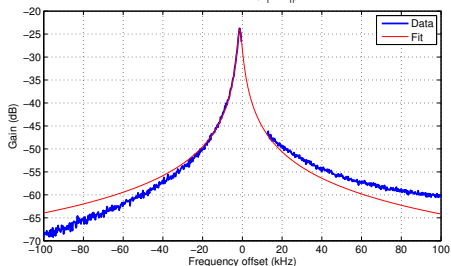
# Wideband Open Loop Transfer Function



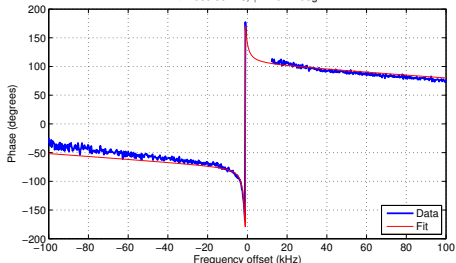
- 200 kHz span;
- Points near the RF frequency show significant scatter;
- For fitting, ignore points in  $-0.5-12.25$  kHz range around RF;
- Increasing errors at large offsets;
- Near the resonance fit seems reasonable.

# Wideband Open Loop Transfer Function

Gain = 0.064,  $Q = 254651$ ,  $(\omega_r - \omega_{pf}) = -1.31$  kHz



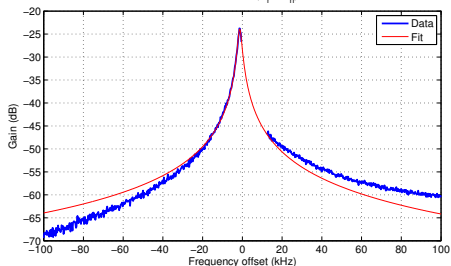
$\tau = 686.862$  ns,  $\phi = 194.2$  deg



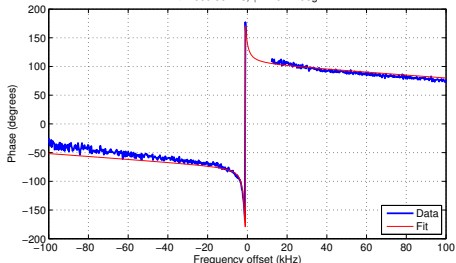
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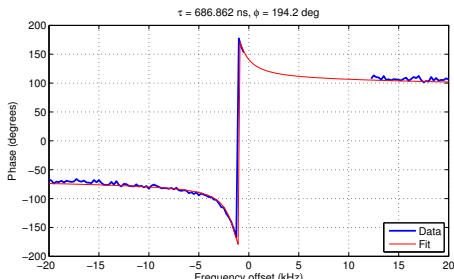
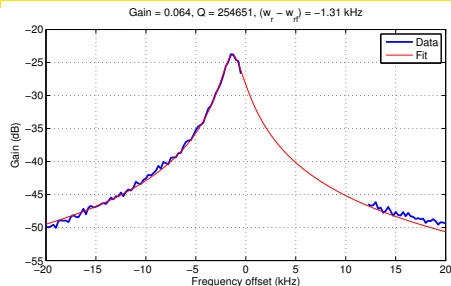


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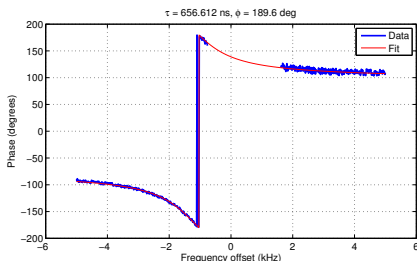
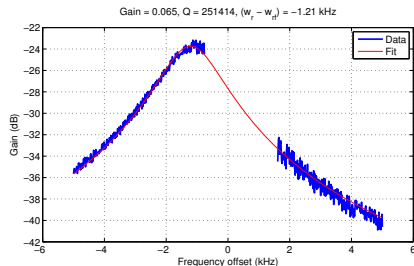
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# Open Loop Transfer Function, 10 kHz Span

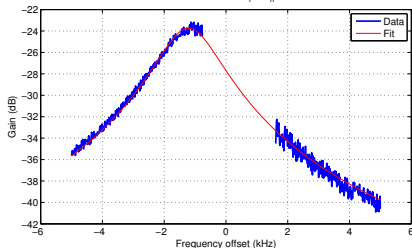


- A good fit (not wideband enough to reliably estimate delay);
- $Q_L$  is 251414, expected 210000;
- Fitted detuning and  $Q_L$  give the loading angle  

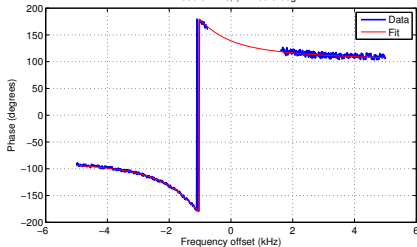
$$\tan^{-1}\left(\frac{2\omega_d Q_L}{\omega_r}\right) = -51^\circ$$
- Suspect at nominal settings might be running with  $-21^\circ$  loading angle, not  $-10^\circ$ .

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$\tau = 656.612$  ns,  $\phi = 189.6$  deg

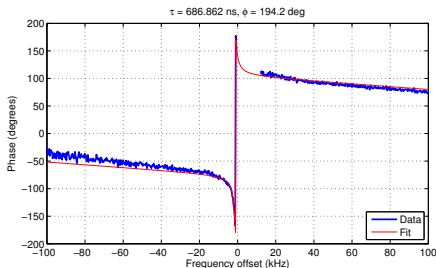
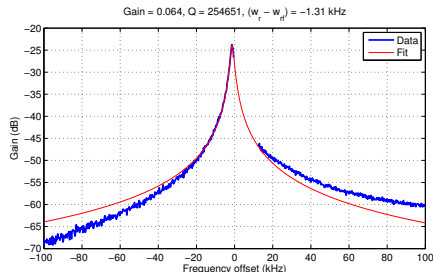


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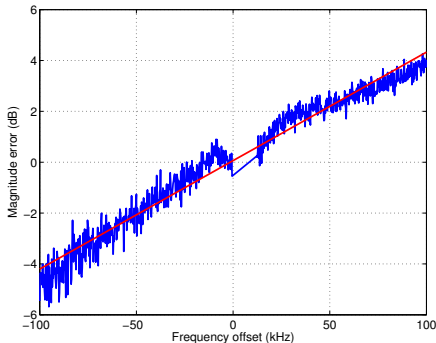
# Correcting Systematics



- Magnitude error is most likely due to RF fundamental feedthrough: cavity response rolls off as  $1/\Delta f^2$  while NWA IF filter rolls off as  $1/\Delta f$ , so error increases with offset;
- $180^\circ$  phase shift across the resonance explains why RF fundamental subtracts below the resonance and adds above;
- Use linear (in dB) correction function;
- Much closer fit.



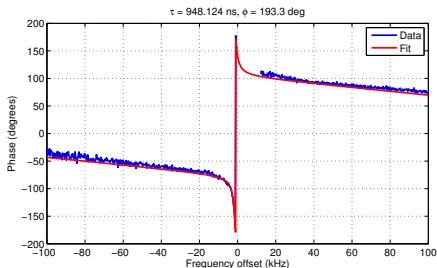
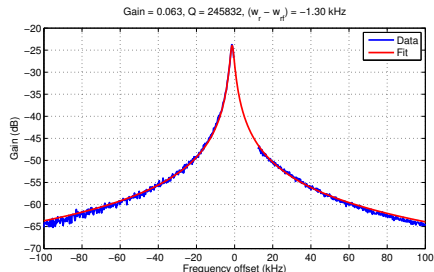
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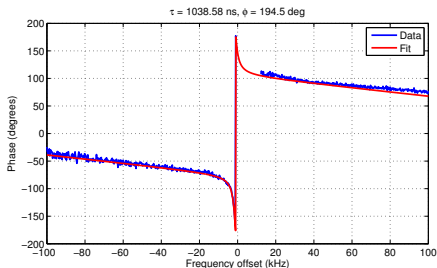
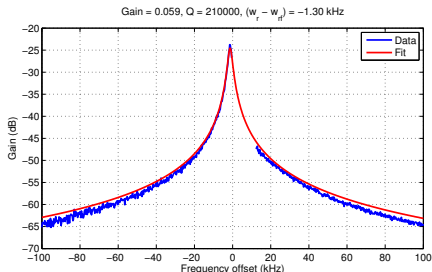
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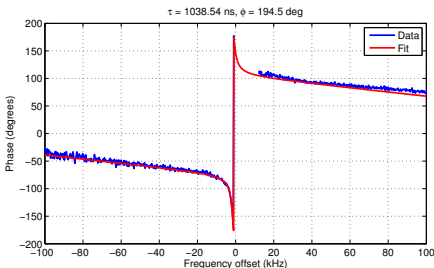
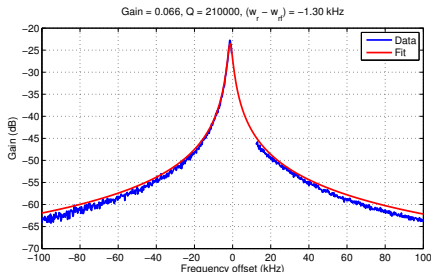


# Fitting and Sensitivity to Q



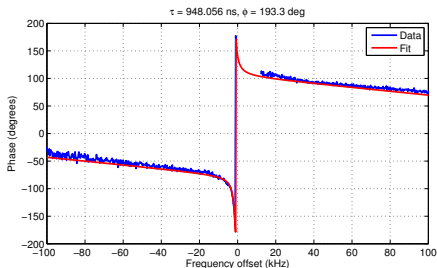
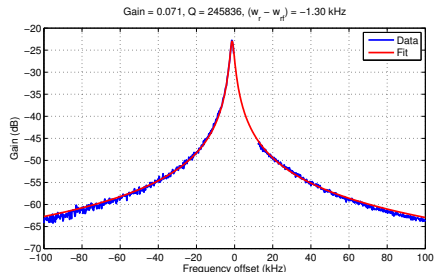
- Forcing  $Q_L = 210000$  worsens the fit to compensated data;
- Even if we use  $Q_L = 210000$  during initial fitting (used to extract linear compensation), final fit is worse;
- Full 5 parameter fit still comes back to higher  $Q_L$ , within  $1.6 \times 10^{-5}$ .

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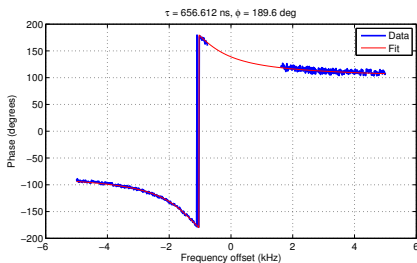
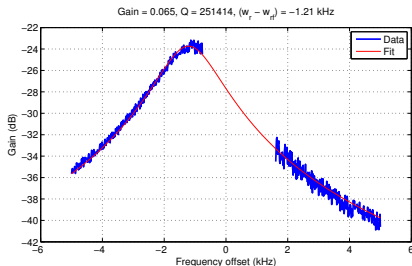
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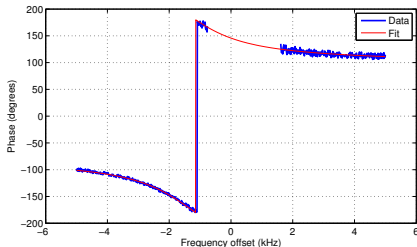
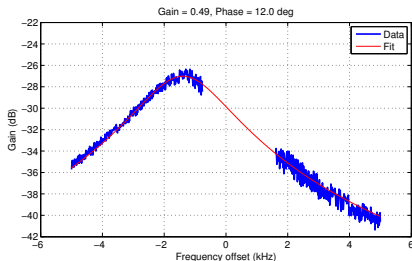
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# Closed Loop Transfer Functions



- Open-loop transfer function;
- Closed-loop transfer functions measured at loop gain settings:
  - 4 V;
  - 5 V;
  - 8 V;
  - 10 V.
- Some saturation at higher control voltages;
- Nominal direct loop gain is 0.5 (50% increase in Robinson beam loading limit).

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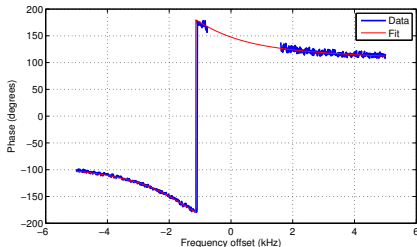
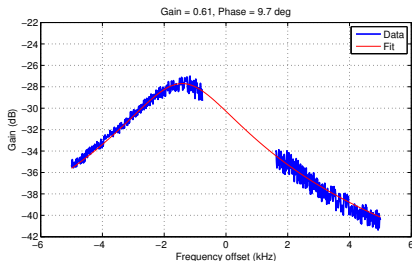


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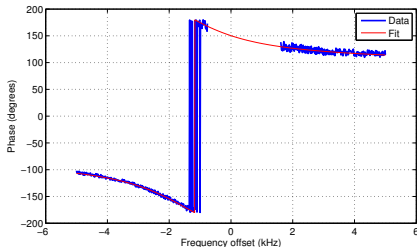
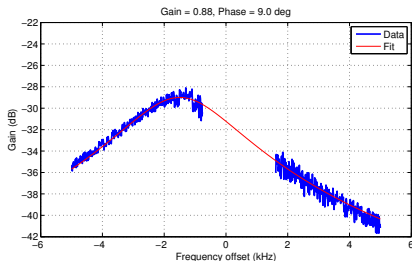
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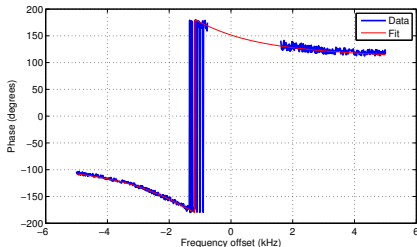
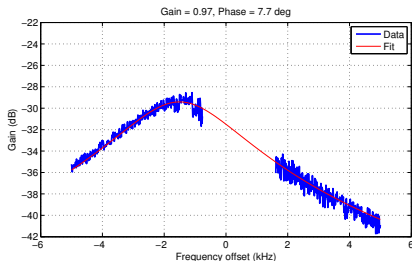
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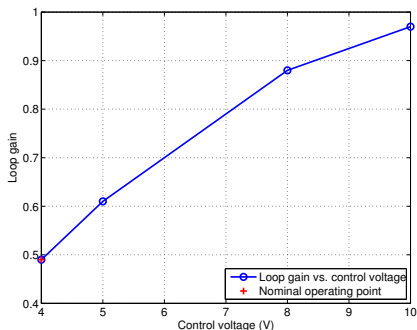
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# Experimental Setup

- Attempted to diagnose beam loss events where RF phase activity has been observed;
- Set up iGp12 (demo unit) and iGp8 to generate abort triggers and capture longitudinal bunch-by-bunch data during the abort:
  - iGp8 connected to a front-end channel tuned for amplitude detection of the BPM sum signal;
  - Bunch-by-bunch feedback filters are configured to differentiate bunch currents with 105 turn delay;
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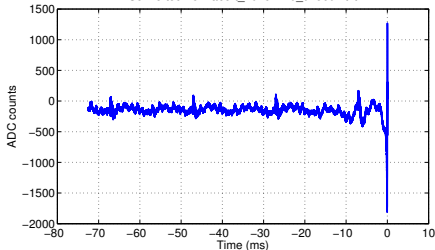
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  - Pre-trigger acquisition feature of iGp12 is used to capture the motion both before and after the trigger.
- Set up automatic abort data readout, ran overnight.

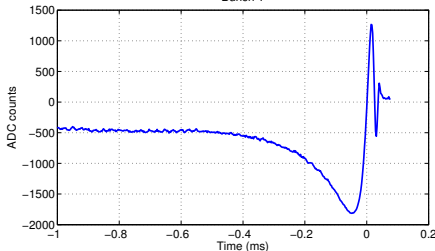


# Beam Loss Event

Converted from abort\_20161210\_075607.txt



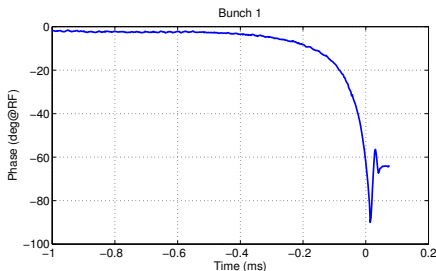
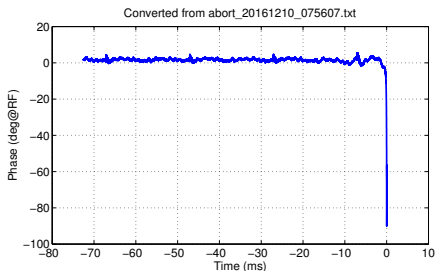
Bunch 1



- What looks like oscillation is actually phase wraparound in the 1.5 GHz phase detector;
- Second negative peak is much smaller due to current loss — we are measuring  $i_b \times \sin \phi_b$ ;
- Full  $360^\circ$  oscillation provides all the necessary information to extract the phase signal;
- All bunches move together.



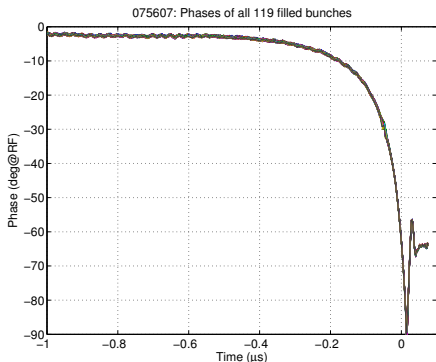
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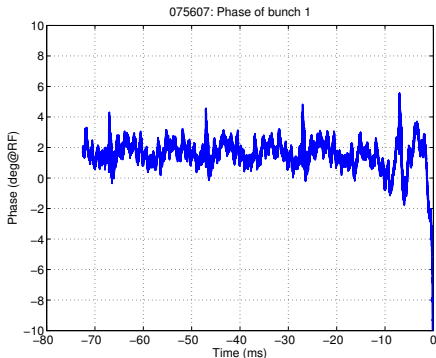


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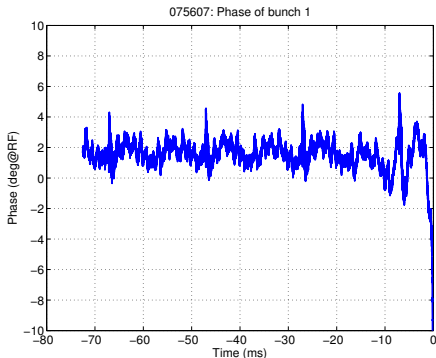
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- Excitations every 20 ms;
- Fairly large steady-state excursions ( $5^\circ$  peak to peak,  $0.6^\circ$  RMS);
- Excitations seem to get bigger just before the abort, could be a coincidence;
- Step excitation (HVPS SCRs?);
- Synchrotron oscillation after a step.

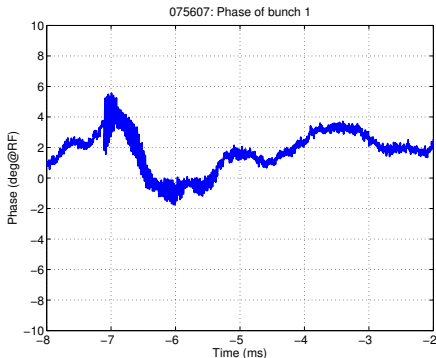
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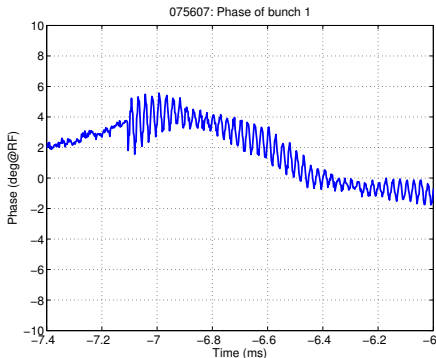


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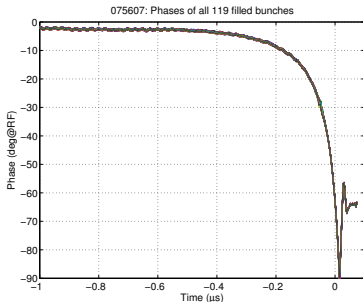
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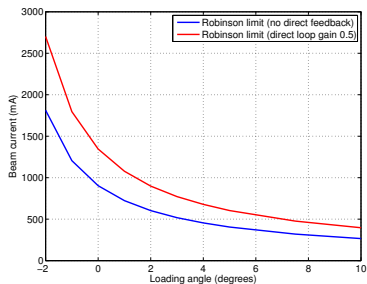
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# Beam Loss: Analysis



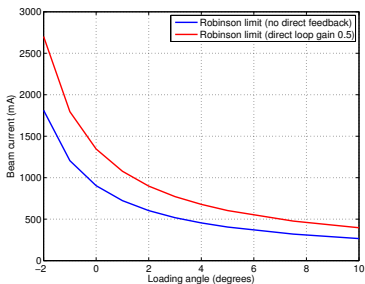
- Exponential beam phase runaway is a typical signature of high beam loading Robinson limit;
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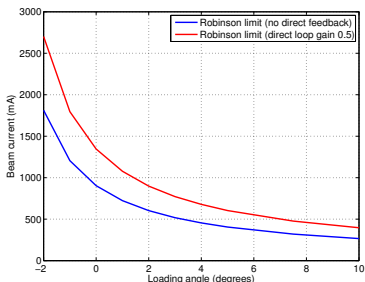
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- With loading angle of  $-10^\circ$  (or even  $-21^\circ$ ) there should be no beam loading limit;
- Is it possible the loading angle is wandering during operation?
- Small positive angle (3-4 degrees) are consistent with loss events observed;
- Increasing direct loop gain to 0.96 (10 V) should provide a 30% higher margin, a good test of the hypothesis;
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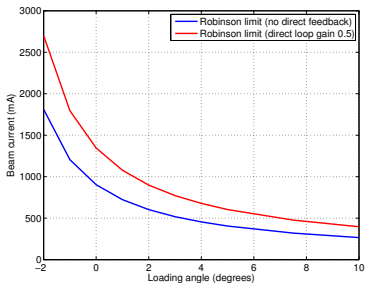
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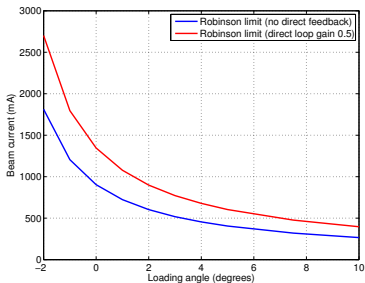
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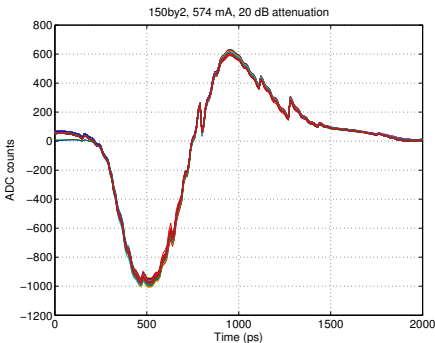


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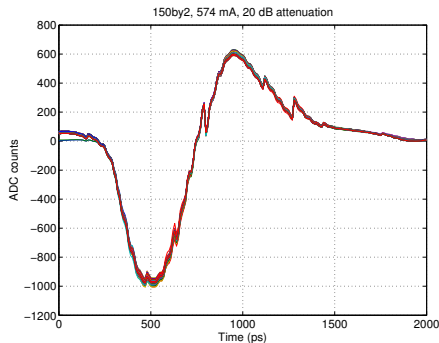
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- Uniform fill of 150 bunches, 4 ns spacing;
- Time sweep generated by adjusting digital delay line with 10 ps resolution;
- Jumps in the sweep correspond to binary transitions — delay stages are not perfect 10-20-40-80-160-320-640-1280 ps;
- Modulated pattern doubles bunch current for 24 bunches in the beginning and 24 bunches in the end of the train;
- AM-to-PM conversion.



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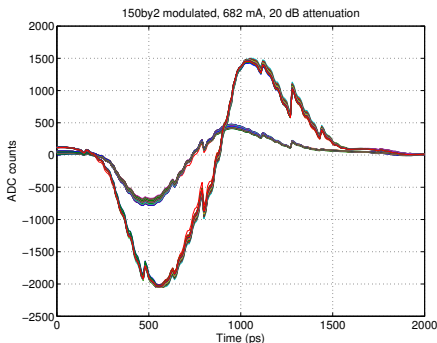


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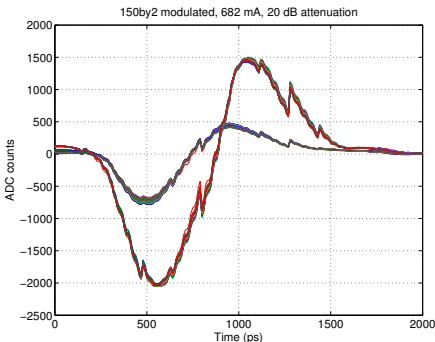
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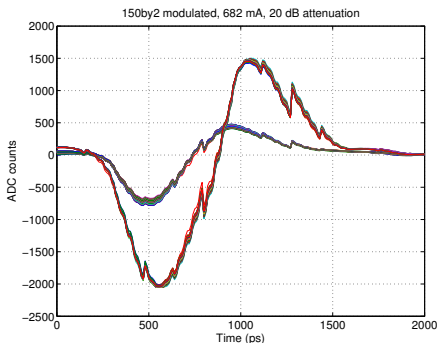
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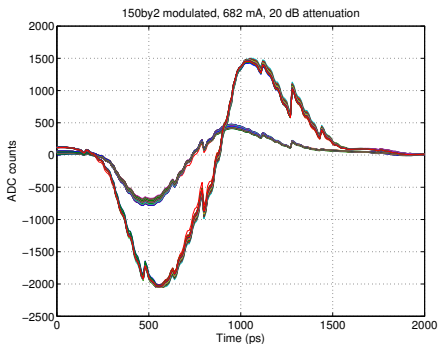


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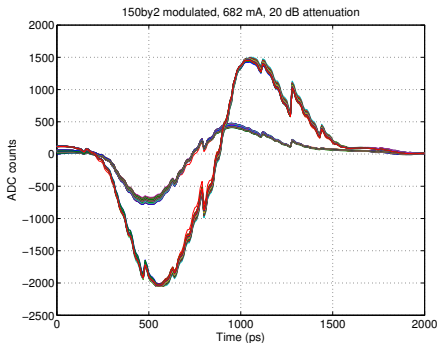
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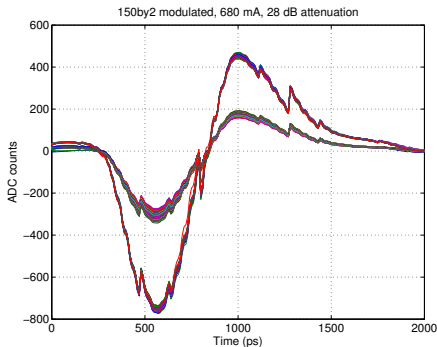
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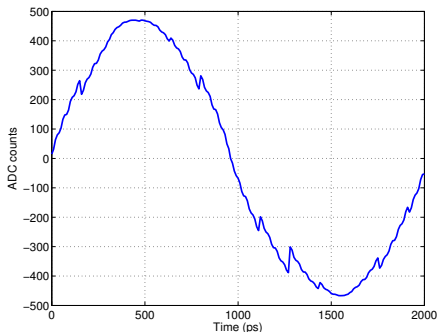
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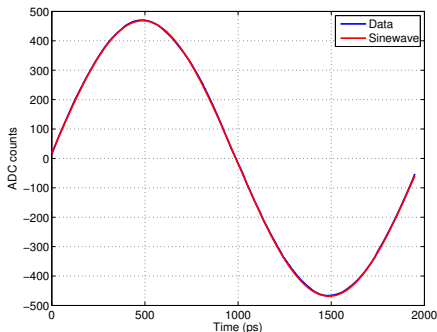


- Calibration based on a measurement of the RF reference signal;
- Optimize delay weights to fit a pure sine wave;

Bit	Nominal	Fit
0	10 ps	10.5 ps
1	20 ps	31.2 ps
2	40 ps	46.6 ps
3	80 ps	89.3 ps
4	160 ps	139.3 ps
5	320 ps	341.9 ps
6	640 ps	646.7 ps
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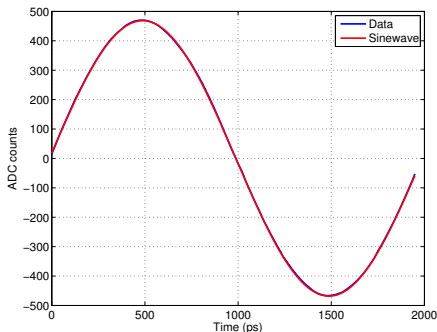
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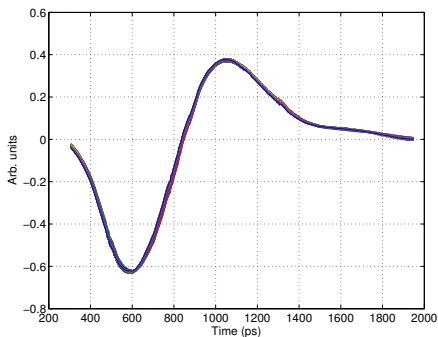


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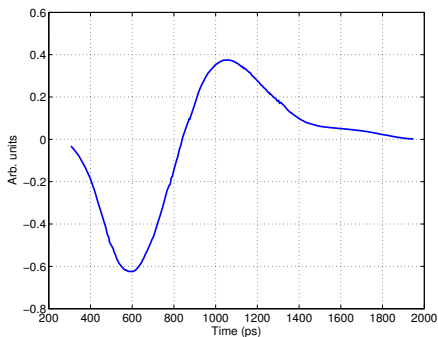
# Bunch Phase and Amplitude Estimation



- Start from individual bunch signals normalized by their peak-to-peak amplitude;
- Calculate average shape signal;
- Fit a 21<sup>st</sup> order polynomial to the average;
- For each bunch perform a two parameter fit: time shift and amplitude scaling;
- Result: bunch-by-bunch currents and phases.

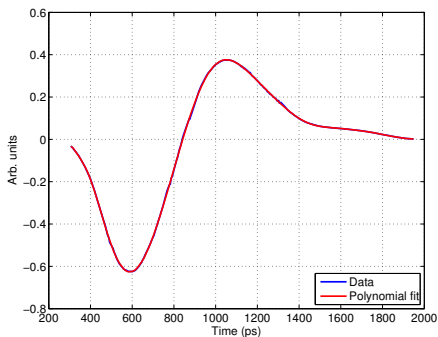


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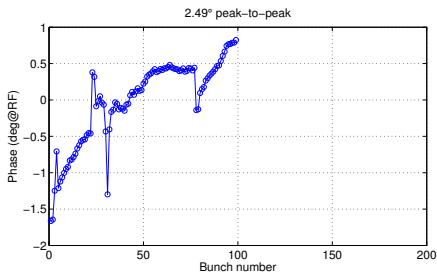
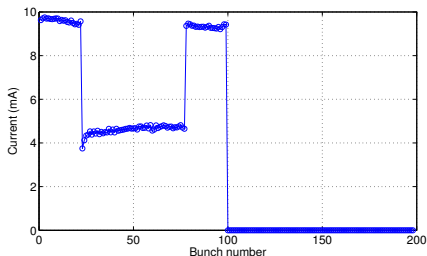
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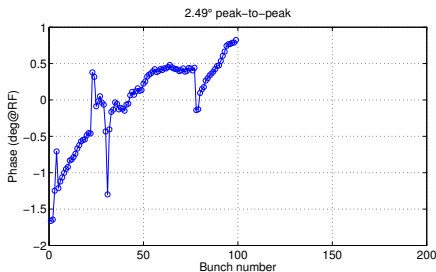
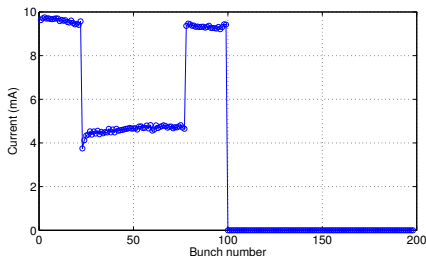
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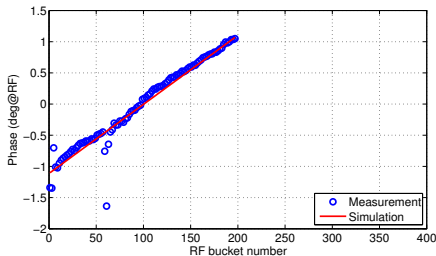
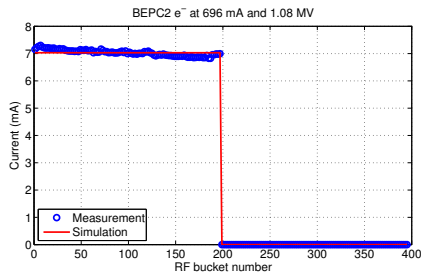
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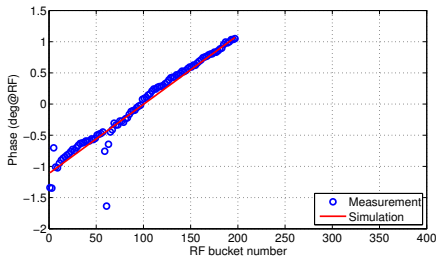
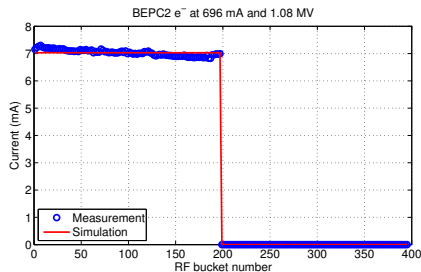
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# Uniform Train: Measurement and Simulation



- To maximize the transient filled half the ring (99 bunches in 4 ns spacing);
- RF voltage reduced to 1.08 MV;
- Calculated transient using Pedersen's small-signal model;
- Feature around bucket 60 is due to an HOM roughly 18 m downstream.

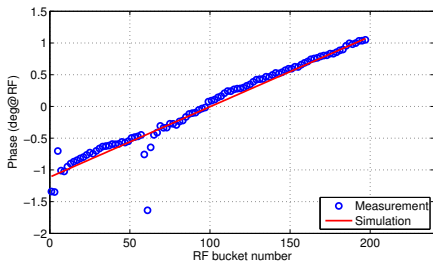
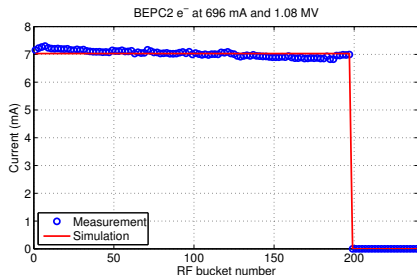
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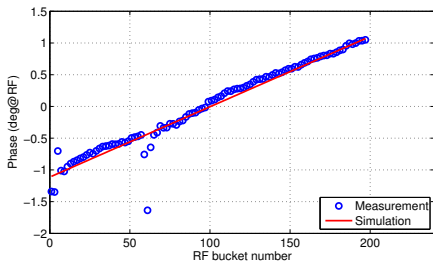
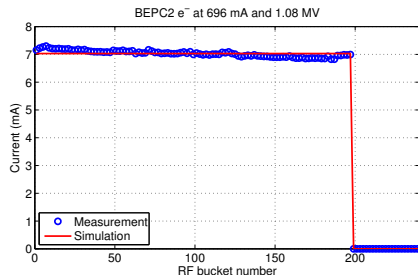


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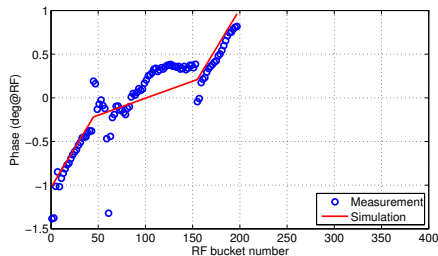
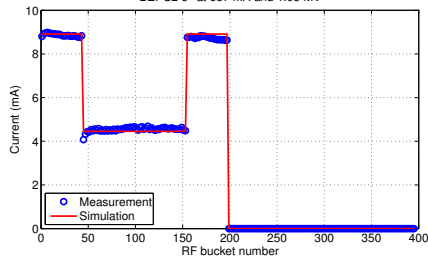
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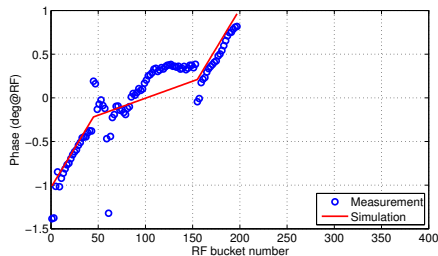
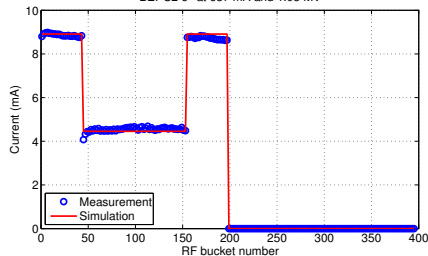
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# Modulated Train: Measurement and Simulation

BEPC2 e<sup>-</sup> at 637 mA and 1.08 MV

- Modulated fill: 22 bunches at the beginning and the end of the train at twice the current;
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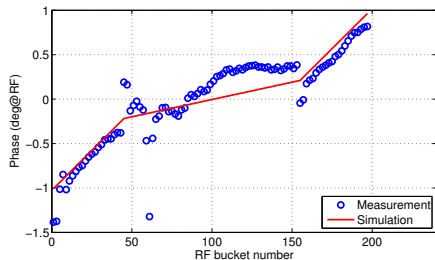
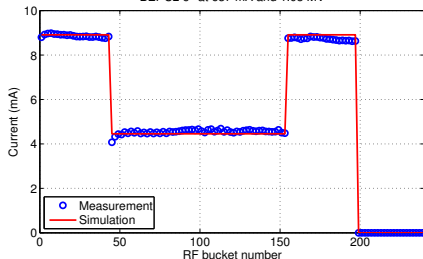
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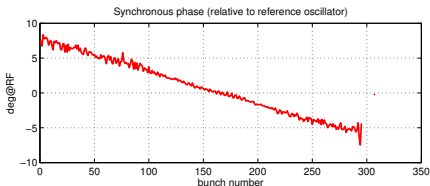
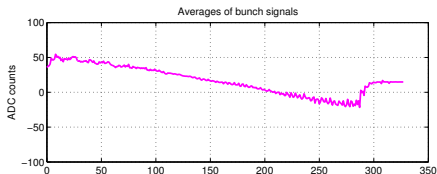
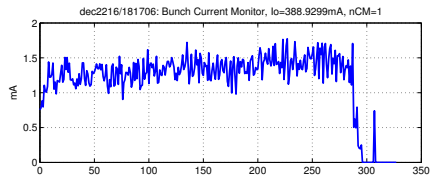


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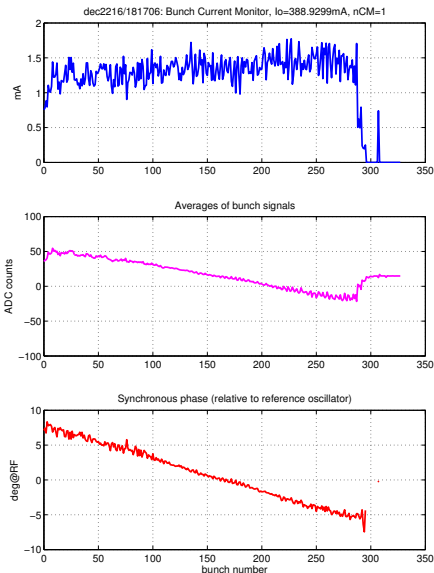
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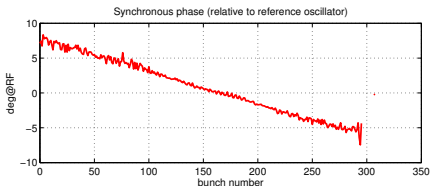
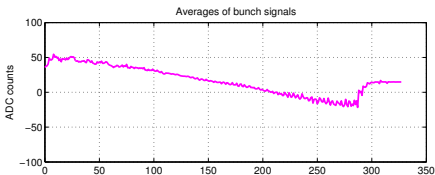
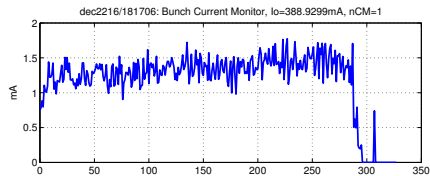
- Nominal fill pattern at the ALS, reduced beam current (388 mA instead of 500 mA);
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  - 15.8 degrees peak-to-peak;
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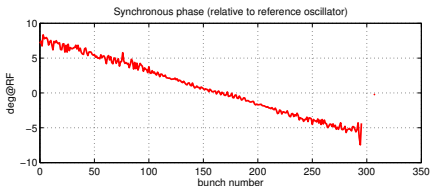
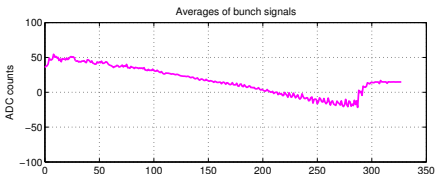
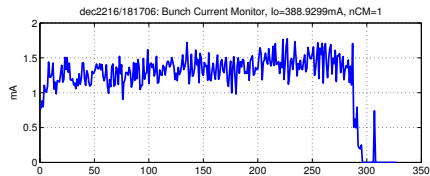
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